

MICHAEL BAKER, JR., INC.

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OHIO RIVER BASIN

NEAL DAM WASHINGTON COUNTY, COMMONWEALTH OF PENNSYLVANIA NDI No. PA 00494 PennDER No. 63-68

PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM

Neal Dam (NDI Number PA-004945 Para DER Number 63-68), Ohio River Basins Eranch of Chartiers Ereek, Washington Countys Pennsylvania Phase I Inspection Reports

Prepared for: DEPARTMENT OF THE ARMY

Baltimore District, Corps of Engineers Baltimore, Maryland 21203

Prepared by:

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PREFACE

This report is prepared under guidance contained in the "Recommended Guidelines for Safety Inspection of Dams," for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I Inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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PHASE I REPORT NATIONAL DAM INSPECTION PROGRAM

Neal Dam, Washington County, Pennsylvania NDI No. PA 00494, PennDER No. 63-68 Tributary of Chartiers Creek Inspected 6 December 1979

ASSESSMENT OF GENERAL CONDITIONS

Neal Dam, owned and operated by Vernon C. Neal, is classified as a "Small" size - "Significant" hazard dam. The dam was found to be in good overall condition at the time of inspection.

Hydraulic/hydrologic evaluations, performed in accordance with procedures established by the Baltimore District, Corps of Engineers, for Phase I Inspection Reports, revealed that the spillway will pass the 100-year flood without overtopping the dam. A spillway design flood (SDF) in the range of the 100-year flood to the 1/2 Probable Maximum Flood (1/2 PMF) is required for Neal Dam. The 100-year flood was chosen because the dam is on the low side of the "Small" size category. The spillway is therefore considered "adequate."

Several minor items of remedial work should be performed by the owner as soon as practicable. These include:

- 1) Clean and seal the cracks in the spillway structure.
- 2) Repair the erosion around both sides of the end of the spillway structure and fill the voids under both sides of the end of the chute slab.
- 3) Raise the embankment/abutment on both sides of the spillway to a minimum Elevation of 1114.2 feet Mean Sea Level (M.S.L.) (top of the spillway walls). It is further recommended that the owner should raise these areas to the average top of dam (Elevati n 1115.5 feet M.S.L.).
- 4) Remove the trees and tree roots from the embankment and have the excavated area regraded and recompacted.

In addition, the following operational measures are recommended to be undertaken by the owner:

1) Develop a detailed emergency operation and warning system.

NEAL DAM

- 2) During periods of unusually heavy rain, provide around-the-clock surveillance of the dam.
- 3) When warning of a storm of major proportions is given by the National Weather Service, the owner should activate the emergency operation and warning system.

It is further recommended that formal inspection, maintenance, and operation procedures and records be developed and implemented. As a part of the formal inspection, the saturated condition of the downstream area of the embankment should be observed and the condition recorded. Also, the joints and cracks in the spillway should be observed and the separation recorded.

Submitted by:

MICHAEL BAKER, JR., INC.

John A. Dziubek, P.E. Engineering Manager-Geotechnical

Date: <u>25 March 1980</u>

Approved by:

JOHN A. DZIUBEK

DEPARTMENT OF THE ARMY
BALTIMORE DISTRICT, CORPS OF ENGINEERS

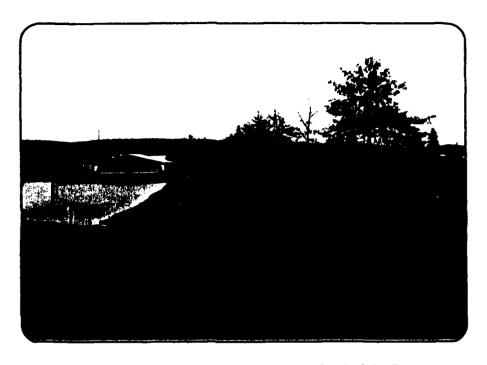
JAMES W. PECK

Colonel, Corps of Engineers

District Engineer

Date: 29 April 1980

NEAL DAM



Overall View of the Upstream Slope and Crest of the Dam from the Right Abutment



Overall View of the Downstream Slope of the Dam from the Right Abutment

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PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM NEAL DAM NDI No. PA 00494, PennDER No. 63-68

SECTION 1 - PROJECT INFORMATION

1.1 GENERAL

- a. Authority The Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of inspection of dams throughout the United States.
- b. <u>Purpose of Inspection</u> The purpose of the inspection is to determine if the dam constitutes a hazard to human life or property.

1.2 DESCRIPTION OF PROJECT

a. Description of Dam and Appurtenances - Neal Dam is an irrigation and recreation facility owned and operated by Mr. Vernon C. Neal. The dam is an earthfill embankment constructed primarily of clay and topsoil for the outer portion of the downstream slope. The dam has a maximum height of 25.6 feet and a crest length of 491 feet. The design drawings show a 12 foot wide clay cut-off trench extending two feet into underlying sandstone. The downstream slope is 5.5H:lV (Horizontal to Vertical) and the upstream slope is 3H:lV. The upstream slope is covered with riprap to within 2 feet of the crest of the dam.

The spillway, located at the right abutment of the dam, is 20 feet wide. The spillway structure extends 10 feet upstream of the location of the spillway crest. The spillway crest is at Elevation 1110.3 feet Mean Sea Level (M.S.L.) and consists of three courses of cinder block placed on the concrete channel slab to form a broad crested The channel slab is at Elevation +1108 feet M.S.L. and was originally designed to function as the normal pool level for the reservoir. The flow through the spillway after passing over the weir will travel approximately 76 feet downstream from the weir before turning to the left and passing over a 6 foot vertical drop. Additional drops of 6 feet and 3 feet are located an additional 30 and 55 feet downstream, respectively. The flow then discharges in a natural earth plunge pool.

The outlet works are located approximately 90 feet to the left of the spillway structure and consist of an 18 inch corrugated metal outlet pipe, a gate valve at the upstream end of the 18 inch corrugated metal pipe, and a junction box approximately 50 feet downstream of the toe of the embankment. An 8 inch V.C.P. carries the discharge from the junction box to the downstream channel.

- b. Location Neal Dam is located in South Franklin Township, Washington County, Pennsylvania, and is approximately 3200 feet southwest of Lagonda, Pennsylvania. The coordinates of the dam are N 40° 06.8', W 80° 17.6'. It can be found on Prosperity, Pennsylvania, USGS 7.5 minute topographic quadrangle.
- c. Size Classification The maximum height of the dam is 25.6 feet and the reservoir volume to the top of the dam is 156 acre-feet at Elevation 1115.5 feet M.S.L. Therefore, the dam is in the "Small" size category.
- d. Hazard Classification There are four secondary roads located below the dam that would be damaged in the event of a rapid discharge of the water behind the dam. In addition to the secondary roads, there are several homes located along Chartiers Creek in Lagonda, Pennsylvania that may suffer economic damage; however, loss of life is unlikely. Therefore, Neal Dam is considered in the "Significant" hazard category.
- e. Ownership The dam and reservoir are owned and operated by Mr. Vernon Neal, Lone Pine Ranch, Lagonda RD #6, Washington, Pennsylvania 15301.
- f. Purpose of the Dam The dam and reservoir are used for irrigation and fishing.
- g. Design and Construction History The dam was designed by Mr. Louis W. Reid, P.E. in 1957, and was built by Mr. Vernon Neal. The construction was started sometime in the fall of 1957 and was completed in December 1957.
- h. Normal Operating Procedures Normal pool Elevation is 1110.32 feet M.S.L. and is maintained by the weir on the spillway. However, the water level drops 5 to 6 feet by late summer due to the lake being used for irrigation purposes. Every fall

the lake is drawn down 3 to 4 feet below the crest of the weir.

1.3 PERTINENT DATA

a.	Drainage Area (square miles) -	0.65
b.	Discharge at Dam Site (c.f.s.) -	
	Maximum Flood - Total Ungated Spillway Capacity	Unknown
	(El. 1113.6 ft.) -	510
c.	<pre>Elevation (feet above M.S.L.) -</pre>	
	Design Top of Dam - Minimum Top of Dam - Average Top of Dam - Normal Pool (Crest of Weir) - Maximum Design Pool - Outlet Pipe -	1116.0 1113.6 1115.5 1110.3 1114.0
	Invert at Entrance ¹ - Invert at Exit - Streambed at Toe of Dam - Maximum Tailwater -	1093 1088.7 1088 <u>+</u> Unknown
d.	Reservoir (feet) -	
	Length of Maximum Pool (El. 1115.5 ft.) - Length of Normal Pool	1700
	(Ĕl. 1110.3 ft.) -	1650
e.	Storage (acre-feet) -	
	Top of Dam (El. 1115.5 ft.) - Normal Pool (El. 1110.3 ft.) -	156 90
f.	Reservoir Surface (acres) -	
	Top of Dam (El. 1115.5 ft.) - Normal Pool (El. 1110.3 ft.) -	13.9 10.5

TEstimated.

g. Dam -

Type -	Earthfill
Length (feet)2-	embankment 491
Height (feet) - Design -	28.0
Field -	25.6
Top Width (feet) -	30
Side Slope - Upstream -	3H:1V
Downstream -	5.5H:1V

Zoning - The original embankment design (see Plate 3) called for a clay fill embankment to be constructed with 3H:lV upstream slope and 2H:lV downstream slope to El. 1114.0 ft. The remaining downstream embankment and two feet of fill on the embankment crest was to be constructed of compacted topsoil. The actual embankment was constructed with a 5.5H:lV downstream slope and, therefore, the actual zoning is not known.

Cut-off - A 12 foot minimum compacted clay cut-off trench is shown on the design plans (see Plate 3) extending approximately 2 feet into underlying sandstone or approximately 8.5 feet below original ground surface for most of the valley bottom.

Grout Curtain - None

Drains - According to the owner's representative,
field drains were installed in the downstream toe area. However, the location or
installation (design) of these drains was
not recorded.

h. Diversion and Regulating Tunnel - None

i. Spillway -

Type -	Broad crested
	weir
Length of Crest Perpendicular	
to Flow (feet) -	20.0
Crest Elevation (feet M.S.L.) -	1110.3
Gates -	None
structure) is spillway weir section is th	10 foot long approach of the spillway upstream from the . Upstream of this e riprap-lined junction abutment and dam

²Estimated from field survey. The design plans show the length of dam as 560 feet.

- Downstream Channel Downstream of the spillway weir the channel (spillway structure) continues straight in plan view for approximately 76 feet before angling to the left and passing over a 6 foot vertical drop.

 Approximately 30 feet downstream is another 6 foot vertical drop in the channel. An additional 25 feet downstream from the second step is the end of the spillway structure which has a 3 foot vertical drop. The spillway flow then discharges into a natural earth plunge pool.
- j. Regulating Outlets The outlet works consist of an 18 inch corrugated metal pipe with a gate valve at the upstream end. Downstream from the toe of the embankment the 18 inch corrugated metal pipe discharges into a junction box. The flow is then carried by an 8 inch V.C.P. to the downstream channel.

SECTION 2 - ENGINEERING DATA

2.1 DESIGN

Neal Dam was designed by Louis W. Reid, P.E. and Arthur E. Tennyson, R.A. for Mr. Vernon C. Neal. The following information was reviewed for the inspection report:

- The design drawings entitled, "Dam Over a Branch of Chartiers Creek" designed by Louis W. Reid, P.E. and Arthur E. Tennyson, R.A., dated 9 August 1957.
- 2) Letter to Mr. Vernon C. Neal from the Division of Dams and Encroachments outlining certain items of design that needed to be revised.
- 3) Revision of design drawings entitled, "Dam Over a Branch of Chartiers Creek" designed by Louis W. Reid, P.E. and Arthur E. Tennyson, R.A., dated 21 August 1957.
- 4) Application and Permit for Construction from the Pennsylvania Department of Environmental Resources (PennDER).
- 5) Construction progress reports made by Mr. Louis W. Reid, P.E., during construction of the dam.
- 6) A report by an Engineer of the Division of Dams and Encroachments, dated 21 September 1961.
- 7) Various photos and correspondence.

2.2 CONSTRUCTION

The construction of Neal Dam was completed by Mr. Vernon C. Neal's construction company. The construction was started sometime in the fall of 1957 and was completed in December 1957.

2.3 OPERATION

Normal pool Elevation is 1110.32 ft. M.S.L. and is maintained by the weir on the spillway. However, the water level drops 5 to 6 feet by late summer due to the lake being used for irrigation. Every fall the lake is drawn down 3 to 4 feet below the crest of the weir to protect the spillway structure from ice. A representative of the owner walks the embankment twice a week

during the summer and twice a month in the winter. The 18 inch gate valve is exercised once a year in the fall to drawdown the lake for the winter.

2.4 EVALUATION

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- a. Availability The information reviewed consisted of the PennDER File No. 63-68 on the dam and information obtained from the owner's representative.
- b. Adequacy The information available is adequate for a Phase I Inspection.
- c. Validity There is no reason or indication at the present time to doubt the authenticity of the available engineering data. However, several changes to the design of the dam made during construction should be noted. These are:
 - 1) The crest width of the embankment is 30 feet. The original design called for a 20 foot crest width.
 - 2) The downstream slope is 5.5H:1V while the original design was 3H:1V.
 - 3) The outlet pipe is 18 inches in diameter rather than the specified 12 inch diameter.
 - 4) The spillway was revised from the original design drawings. See the field sketch in Appendix A for the "as built" plan view of the spillway.
 - 5) The cut-off walls at the spillway were not constructed as designed. Only the two foot long left side cut-off wall was observed.

SECTION 3 - VISUAL INSPECTION

3.1 FINDINGS

- a. General The visual inspection of Neal Dam was performed on 6 December 1979. The pool at the time of the inspection was at Elevation 1107.40 feet M.S.L. and no water was flowing over the weir. At the time of inspection, the dam and its appurtenances were considered to be in good condition. Noteworthy deficiencies observed during the inspections are described briefly in the following paragraphs. The visual inspection check list, field sketch, field sketch of the spillway, top of dam profile, and typical cross-section are given in Appendix A.
- b. Dam The embankment has a good cover of grass which is kept well cut. There are also several pin oaks planted along the downstream crest. No stability problems were discovered, but the soil along the downstream toe area was saturated. The owner's representative reported that this condition only exists during wet falls and wet springs and dries during the drier summer months.
- c. Appurtenant Structures The outlet works appeared to be in fair overall condition. It was found that the 12 inch steel pipe as shown on the construction drawings had been replaced with an 18 inch corrugated metal pipe during construction of the embankment.

The crest of the spillway has been raised by the owner to gain additional storage capacity. Three courses of cinder blocks were placed in the channel to raise the crest approximately 2.3 feet. Throughout this report the spillway crest cited is the weir created by these blocks.

The concrete training walls have several large cracks in them. A couple of construction and expansion joints have partially separated. Some of the concrete in the spillway is honeycombed.

The concrete chute had several large cracks in the slabs. At the bottom of the concrete chute it appeared that the soil from behind both training walls was eroded. On the right side this erosion extended 3 to 4 feet beneath the chute slab and on the right side the void under the chute slab extended 8 or 9 feet back.

- d. Reservoir Area No problems were observed in the reservoir area. The reservoir slopes are primarily moderately sloping pastures and farmlands. Approximately 1500 feet upstream of the reservoir there is a small dam.
- e. Downstream Channel Approximately 300 feet downstream of Neal Dam is a private road; 800 feet below the dam is the confluence of the downstream channel and Chartiers Creek. Below the confluence there are four small bridges which serve secondary roads. It is likely that these bridges would be damaged in the event of excessively rapid discharge. At approximately 3500 feet below the dam is the village of Lagonda. Several residential structures would suffer some economic damage but no loss of life would be expected in the event of a rapid discharge from Neal Dam.

SECTION 4 - OPERATIONAL PROCEDURES

4.1 PROCEDURES

Currently there are no formal written procedures in the event of impending failure of the dam. The condition of the dam is checked twice a week during warm weather and twice a month during the winter. The maintenance building for the golf course is located approximately 200 feet downstream on the right bank of the downstream channel. With this building being this close to the dam, it allows the golf course superintendent to make a quick visual inspection of the dam every day.

The 18 inch gate valve is opened each fall resulting in a drop of the water level 3 to 4 feet below the crest of the spillway.

It is recommended that formal emergency procedures be prepared, prominently displayed, and furnished to all operating personnel.

4.2 MAINTENANCE OF DAM

The maintenance condition of the dam is considered to be fair. There are no formal procedures for evaluating the necessity of maintenance for the dam; however, the golf course superintendent determines what work needs to be performed and schedules the work. It is recommended that formal maintenance procedures be developed and implemented.

4.3 MAINTENANCE OF OPERATING FACILITIES

The 18 inch gate valve is exercised only once a year in the fall to drawdown the lake level 3 to 4 feet below the crest of the weir. It is recommended that formal preventive maintenance schedules be established to assure continued operation.

4.4 WARNING SYSTEM

At the present time, there is no formal warning system or evacuation plan in operation.

4.5 EVALUATION OF OPERATING ADEQUACY

Maintenance of the operating facilities is considered adequate for the functions that they serve.

SECTION 5 - HYDRAULIC/HYDROLOGIC

5.1 EVALUATION OF FEATURES

- a. Design Data PennDER files were reviewed for hydrologic and hydraulic design data. No hydrologic information was available in the files. They did contain one page showing that the maximum non-damaging discharge from the spillway was 772 c.f.s., based on the weir flow equation.
- b. Experience Data There was no information available on the maximum reservoir level or discharge.
- c. <u>Visual Observations</u> The low area on the crest of the dam adjacent to the spillway could have a minor effect on the hydraulic capability of the reservoir. No other conditions were observed at the time of the inspection that would indicate the dam and appurtenant structures could not operate satisfactorily in the event of a flood.
- d. Overtopping Potential - Neal Dam is classified as a "Significant" hazard - "Small" size dam requiring evaluation for a spillway design flood (SDF) in the range of the 100-year flood to the 1/2 Probable Maximum Flood (1/2 PMF). Since the dam is on the low end of the small size category, the 100-year flood was chosen as the SDF. Using regression equations developed by the Pittsburgh District of the Corps of Engineers for the Ohio River Basin, the peak inflow to the impoundment for the 100year flood was calculated to be 450 c.f.s. spillway can safely pass a flow of 510 c.f.s. without overtopping. Because the peak inflow to the impoundment is less than the spillway capacity, the spillway of the dam is capable of passing the SDF without overtopping.
- e. Spillway Adequacy The dam, as outlined in the above analysis, is capable of passing the 100-year flood without overtopping. The spillway is therefore considered adequate according to the recommended criteria.

SECTION 6 - STRUCTURAL STABILITY

6.1 EVALUATION OF STRUCTURAL STABILITY

a. Visual Observations - No distress or seepage was observed on the embankment during the visual inspection. The saturated condition of the toe area of the embankment is not considered to be the result of steady state seepage through the embankment. In addition, the presence of this moisture does not indicate concern relative to the stability of the 5.5H:lV downstream slope. It is recommended that this area be periodically examined as a part of future inspections of the dam.

The cracks observed in the concrete of the spillway structure are not considered to adversely affect the structural stability of the spillway at this time. The opening of a couple of the construction joints in the spillway training walls is an undesirable condition; however, it is estimated that the stability of these walls is not in jeopardy at this time. It is recommended that cracks and joints be examined during the annual inspections and the amount of separation recorded.

- b. Design and Construction Data Design calculations were not available for review. Because of the low height of the dam, the moderate slopes and total width of the embankment, and because no signs of distress or steady state seepage was observed; no further stability analysis is deemed necessary for this Phase I Inspection Report.
- c. Operating Records Nothing in the operational information indicates concern relative to the structural stability of the dam.
- d. Post-Construction Changes The modification of the spillway by placing the additional 2.3 foot high cinder block wall in the channel decreases the amount of available flood storage in the reservoir and increases the possibility of overtopping the embankment; however, the spillway has been shown in Section 5 as capable of passing the recommended SDF. No other changes adversely affecting the structural stability of the dam have been performed.

e. Seismic Stability - The dam is located in Zone lon the "Seismic Zone Map of the Contiguous United States," Figure 1, page D-30, "Recommended Guidelines for Safety Inspection of Dams." This is a zone of minor seismic activity, and therefore, further consideration of the seismic stability is not warranted.

SECTION 7 - ASSESSMENT, RECOMMENDATIONS/REMEDIAL MEASURES

7.1 DAM ASSESSMENT

a. Safety - Neal Dam was found to be in good overall condition at the time of inspection. Neal Dam is a "Significant" hazard - "Small" size dam requiring a spillway capacity in the range of the 100-year flood to 1/2 PMF. The 100-year flood was chosen as the SDF because the dam is on the low side of the "Small" size category. As presented in Section 5, the spillway and reservoir are adequate to pass the 100-year flood without overtopping the dam. Therefore, the spillway is considered "adequate."

The saturated condition at the toe of the embankment is considered to be the result of rainfall and not steady state seepage. This condition, at the present time, is not considered to adversely affect the structural stability of the embankment. However, this area should be observed in future inspections and the condition recorded.

Joint separations and cracks in the spillway structure are undesirable, but their condition should not affect the structural stability of the spillway at this time. It is recommended that the joints and cracks in the spillway be observed in future inspections and the condition and amount of separation recorded.

- b. Adequacy of Information The information available and the observations and measurements made during the field inspection are considered sufficient for this Phase I Inspection Report.
- c. <u>Urgency</u> The owner should initiate the action discussed in paragraph 7.2 as soon as practicable.
- d. <u>Necessity for Additional Data/Evaluation</u> No further investigation is necessary.

7.2 RECOMMENDATIONS/REMEDIAL MEASURES

The inspection revealed certain items of remedial work which should be performed by the owner. These include:

1) Clean and seal the cracks in the spillway structure.

- 2) Repair the erosion around both sides of the end of the spillway structure and fill the voids under both sides of the end of the chute slab.
- 3) Raise the embankment/abutment on both sides of the spillway to a minimum Elevation of 1114.2 feet M.S.L. (top of the spillway walls). It is further recommended that the owner should raise these areas to the average top of dam (Elevation 1115.5 feet M.S.L.).
- 4) Remove the trees and tree roots from the embankment and have the excavated area graded and recompacted.

In addition, the following operational measures are recommended to be undertaken by the owner:

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- Develop a detailed emergency operation and warning system.
- During periods of unusually heavy rain, provide around-the-clock survillance of the dam.
- 3) When warning of a storm of major proportions is given by the National Weather Service, the owner should activate the emergency operation and warning system.

It is further recommended that formal inspection, maintenance, and operation procedures and records be developed and implemented. As a part of the formal inspection, the saturated condition of the downstream area of the embankment should be observed and the condition recorded. Also, the joints and cracks in the spillway should be observed and the separation recorded.

APPENDIX A

VISUAL INSPECTION CHECK LIST, FIELD SKETCH, FIELD SKETCH OF THE SPILLWAY, TOP OF DAM PROFILE, AND TYPICAL CROSS-SECTION

Check List Visual Inspection Phase 1

The state of the s

Lat. N 40°06.8' Long. W 80°17.6' Coordinates 35° F. Temperature PA State Weather Overcast, cool County Washington (South Franklin Township) Date of Inspection 6 December 1979 Name of Dam Neal Dam NDI # PA 00494 PennDER # 63-68

M.S.L. 992.10 Tailwater at Time of Inspection ft. M.S.L. 1107.40 ft. Pool Elevation at Time of Inspection

Inspection Personnel:

Owner's Representatives:

John McCellard, Superintendent

Michael Baker, Jr., Inc.:
James G. Uliniski
Jeff Maze
Jeff Quay

James G. Uliniski

Recorder

CONCRETE/MASONRY DAMS - Not Applicable

	REMARKS OR RECOMMENDATIONS
	OBSERVATIONS
Name of Dam: NEAL DAM	VISUAL EXAMINATION OF

LEAKAGE

STRUCTURE TO ABUTMENT/EMBANKMENT JUNCTIONS

DRAINS

WATER PASSAGES

FOUNDATION

CONCRETE/MASONRY DAMS - Not Applicable

Name of Dam: NEAL DAM		
NDI # PA 00494	I	
VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SURFACE CRACKS CONCRETE SURFACES		
STRUCTURAL CRACKING		
VERTICAL AND HORIZONTAL		
MONOLITH JOINTS		
CONSTRUCTION JOINTS		

the state of the state of the same that is not been to be a second of the same of the same

EMBANKMENT

Name of Dam: NEAL DAM NDI # PA 00494

REMARKS OR RECOMMENDATIONS OBSERVATIONS VISUAL EXAMINATION OF

SURFACE CRACKS

None

UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE

None

None, except at the end of the spillway structure (see page A-7).

SLOUGHING OR EROSION OF EMBANKMENT AND ABUTMENT SLOPES No problems observed

VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST

None

RIPRAP FAILURES

EMBANKMENT

Name of Dam: NEAL DAM NDI # PA 00494

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
Trees	Pin oaks were observed on approximately 50 ft. spacings along the downstream edge of the crest of the embankment.	The trees and tree roots should be removed and the excavated area graded and recompacted.
JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLWAY AND DAM	No problems observed	

Areas on both side of the outlet were wet and saturated (spongy). The owner's representative reported these areas are typically wet in the spring and fall and after heavy rain showers.	None
ANY NOTICEABLE SEEPAGE	STAFF GAGE AND RECORDER

downstream area; however, location and details of the installation were not recorded. The drains discharge into a small well reservoir located downstream. Field tile drains were installed in the DRAINS

OUTLET WORKS

Name of Dam: NEAL DAM

NDI # PA 00494

REMARKS OR RECOMMENDATIONS The outlet conduit (18 in. C.M.P.) at the junction box downstream was in reasonable condition. The rest of conduit could not be inspected. OBSERVATIONS CRACKING AND SPALLING OF VISUAL EXAMINATION OF CONCRETE SURFACES IN OUTLET CONDUIT

for the gate appeared slightly bent but The valve stem The intake structure is submerged and could not be examined. is operational. INTAKE STRUCTURE

The outlet structure (junction box) was in reasonable condition. The 8 in. V.C.P. from the junction box discharges into the downstream channel.

OUTLET STRUCTURE

OUTLET CHANNEL Not Applicable

The 18 in. gate valve is submerged and could not be examined. The gate valve is normally used every fall to lower the reservoir a few ft. to prevent ice action on the spillway structure.

EMERGENCY GATE

UNGATED SPILLWAY

Name of Dam: NEAL DAM NDI # PA 00494

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OR RECOMMENDATIONS	
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VISUAL EXAMINATION OF

CONCRETE WEIR The weir has been raised by 3 courses of blocks by the owner.

Masonry appeared in good condition.

APPROACH CHANNEL No problems observed

The discharge channel is in good condition except for cracks in the concrete floor and walls.

DISCHARGE CHANNEL

Clean out and seal cracks.

BRIDGE AND PIERS

None

REMARKS OR RECOMMENDATIONS GATED SPILLWAY - Not Applicable OBSERVATIONS NEAL DAM VISUAL EXAMINATION OF Name of Dam: NDI # PA 00494 CONCRETE SILL

APPROACH CHANNEL

DISCHARGE CHANNEL

BRIDGE AND PIERS

GATES AND OPERATION EQUIPMENT

		į
Name of Dam: NEAL DAM NDI # PA 00494	INSTRUMENTATION - None	A-9
VISUAL EXAMINATION	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
Monumentation/surveys		
OBSERVATION WELLS		
Weirs		
Piezometers		
OTHER		

RESERVOIR

NEAL DAM Name of Dam:

NDI # PA 00494

SLOPES

OBSERVATIONS VISUAL EXAMINATION OF

REMARKS OR RECOMMENDATIONS

ջ

The reservoir slopes are mildly sloping. problems were observed.

SEDIMENTATION

Sediment in the deepest spot (near the outlet works) is approximately 15 to 18 in. Some sedimentation has occurred on the upper end of the reservoir.

DOWNSTREAM CHANNEL

Name of Dam: NEAL DAM

NDI # PA 00494

VISUAL EXAMINATION OF

OBSERVATIONS

REMARKS OR RECOMMENDATIONS

CONDITION

(OBSTRUCTIONS, DEBRIS, ETC.)

The downstream channel has a few cattails growing in it immediately downstream from the discharge channel. The remainder of the channel is clear of any type of debris.

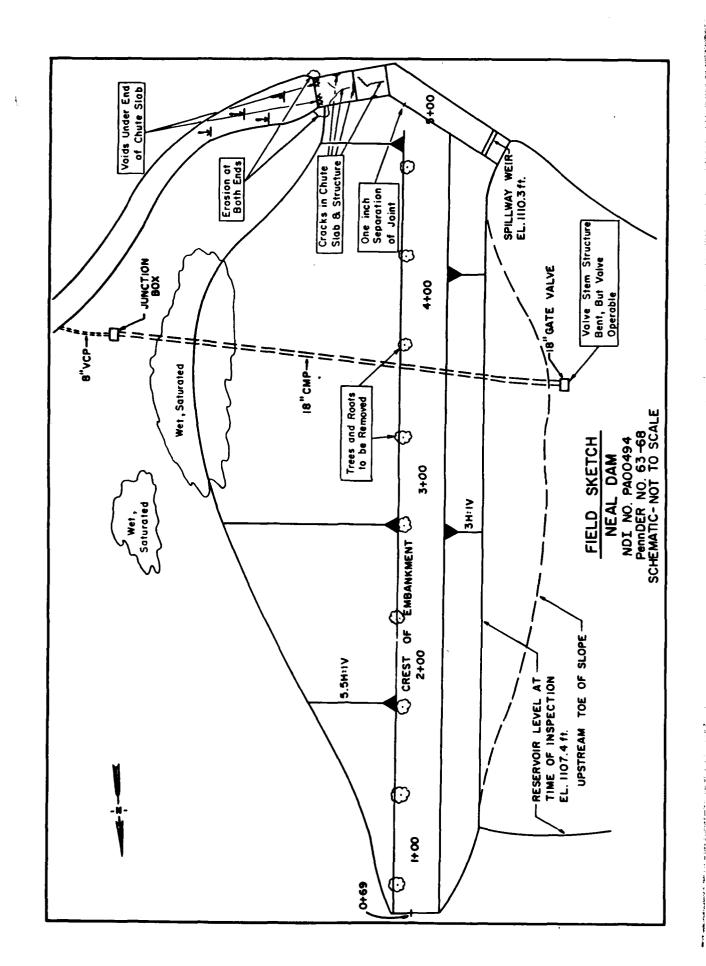
SLOPES

The channel slope is approximately 2.5% from the toe of the dam to the confluence with Chartiers Creek. The channel side slopes are mild and no problems were observed.

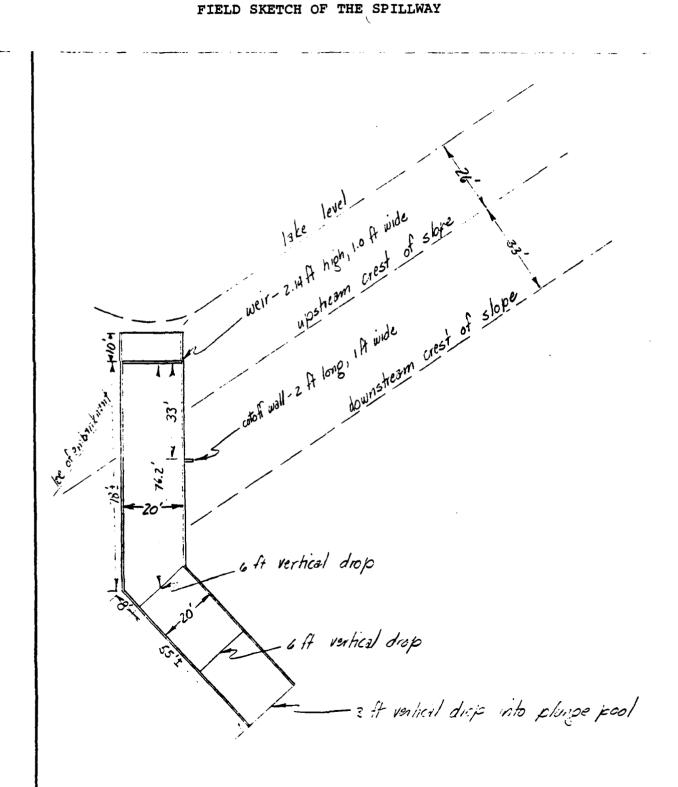
APPROXIMATE NO.

POPULATION

The culvert is a 48 in. diameter C.M.P. Approxto the maintenance building crosses the channel two bridges and downstream from the last bridge with Chartiers Creek. 250 ft. from the confluence downstream is the access road to the golf course and dam. Located 2700 ft. and 3500 ft. approximately 300 ft. downstream from the dam. ship road bridges. Several homes between the are located within the floodplain of Chariers The golf course maintenance building is built imately 800 ft. downstream is the confluence would not suffer any damage. An access road higher than the channel on fill and probably downstream from the confluence are two town-Creek and may suffer economic damage in the event of a dam failure or heavy discharges from the dam.

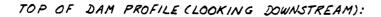


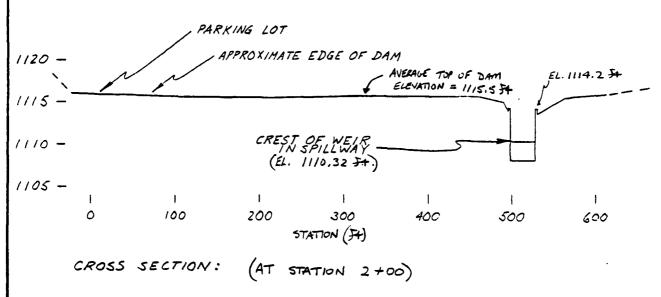
NEAL DAM .

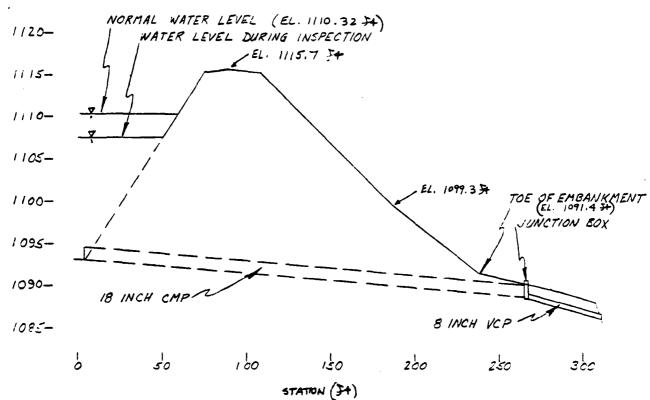


NEAL DAM

TOP OF DAM PROFILE TYPICAL CROSS-SECTION







APPENDIX B

ENGINEERING DATA CHECK LIST

CHECK LIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION

Name of Dam: NEAL DAM
NDI # PA 00494
ITEM REMARKS

PLAN OF DAM	The original design drawing showing the plan of dam has been re- produced and included in this report as Plate 3.
REGIONAL VICINITY MAP	A JSGS 7.5 minute topographic quadrangle, Prosperity, Pennsylvania, was used to prepare the vicinity map which is enclosed in this report as the Location Plan (Plate 1).
CONSTRUCTION HISTORY	The dam was designed by Mr. Louis W. Reid, P.E. and was constructed by Mr. Vernon C. Neal. The construction started in the fall of 1957 and was completed in December of 1957.
TYPICAL SECTIONS OF DAM	An original design drawing cross-section is shown on Plate 3 of this report. A typical cross-section, measured during the visual inspection, is included in Appendix A.
HYDROLOGIC/HYDRAULIC DATA	No information available

OUTLETS - PLAN and DETAILS See Plate 3 of this report.

- CONSTRAINTS None

- DISCHARGE RATINGS No information available

RAINFALL/RESERVOIR RECORDS

Rainfall records are kept by the superintendent of maintenance of the golf course. Reservoir records are not kept.

Name of Dam: NEAL DAM NDI # PA 00494

ITEM

REMARKS

DESIGN REPORTS

None available

GEOLOGY REPORTS

No information was available. The regional geology is included in this report as Appendix F.

DESIGN COMPUTATIONS
HYDROLOGY & HYDRAULICS
DAM STABILITY
SEEPAGE STUDIES

None available

MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD

Four test pits were dug along the centerline axis of the dam. The location and results of these test pits are shown on Plate 4 of this report.

POST-CONSTRUCTION SURVEYS OF DAM

None

BORROW SOURCES

According to the owner's representative, the borrow for the dam came from the left abutment hillside.

.

> NEAL DAM Name of Dam:

ITEM

NDI # PA 00494

MONITORING SYSTEMS

None

REMARKS

MODIFICATIONS

The crest of the spillway was raised 3 ft. with a cinder block wall. A gasline was installed crossing the downstream slope from the right downstream toe to the left crest of the slope. The gasline was placed 2 ft. below grade.

No information available

HIGH POOL RECORDS

POST-CONSTRUCTION ENGINEERING STUDIES AND REPORTS

An inspection report by a representative of PennDER on 25 September 1961. This report is available in the PennDER file.

PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION

REPORTS

None

MAINTENANCE OPERATION RECORDS

the summer and approximately twice a month in the winter. The maintenance building for the golf course is located on the right hillside below the dam and people are usually there year Formal maintenance and operation records are not kept. Mr. McCelland walks the embankment approximately twice a week in round, therefore, any unusual occurrence at the dam would probably be observed. Name of Dam: NEAL DAM NDI # PA 00494

ITEM SPILLWAY PLAN,

REMARKS

SECTIONS,

and DETAILS

See Plates 3 and 4 of this report.

OPERATING EQUIPMENT PLANS & DETAILS

No details available

CHECK LIST HYDROLOGIC AND HYDRAULIC DATA ENGINEERING DATA

DRAINAGE AREA CHARACTERISTICS: 0.65 sq.mi.
Illo.ft.
ELEVATION TOP NORMAL POOL (STORAGE CAPACITY): (90 acft.)
1115.5 ft.
ELEVATION TOP FLOOD CONTROL POOL (STORAGE CAPACITY): (156 acft.)
ELEVATION MAXIMUM DESIGN POOL: 1114.0 ft.
ELEVATION TOP DAM: 1113.6 ft. (minimum), 1115.5 ft. (average)
CREST: Spillway
a. Elevation 1110.32 ft.
h Type Sharp-crested congrete weir in restangular congrete
c. Width of Crest Parallel to Flow 1 ft channel
d. Length of Crest Perpendicular to Flow 20 ft.
e. Location Spillover At right abutment of dam f. Number and Type of Gates None
1. Number and Type of Gates None
OUTTET WORKS. Beside for descending manager
OUTLET WORKS: Facilities for dewatering reservoir
a. Type 18 in dia C M P feeding into 8 in dia V C P
The state of the s
b. Location Near centerline of embankment
c. Entrance inverts <u>El. 1093 ft. (estimated)</u>
d. Exit inverts El. 1088.7 ft. (18 in. C.M.P.), El. 1087.4 ft.
e. Emergency draindown facilities Gate valve at (8 in. V.C.P.)
upstream end of 18 in. C.M.P.
HYDROMETEOROLOGICAL GAGES: None installed
a. Type
b. Location
c. Records
MAXIMUM NON-DAMAGING DISCHARGE Unknown
معتبر والمنظل في المنظم والمنظم والمنظ

APPENDIX C

PHOTOGRAPH LOCATION PLAN AND PHOTOGRAPHS

DETAILED PHOTOGRAPH DESCRIPTIONS

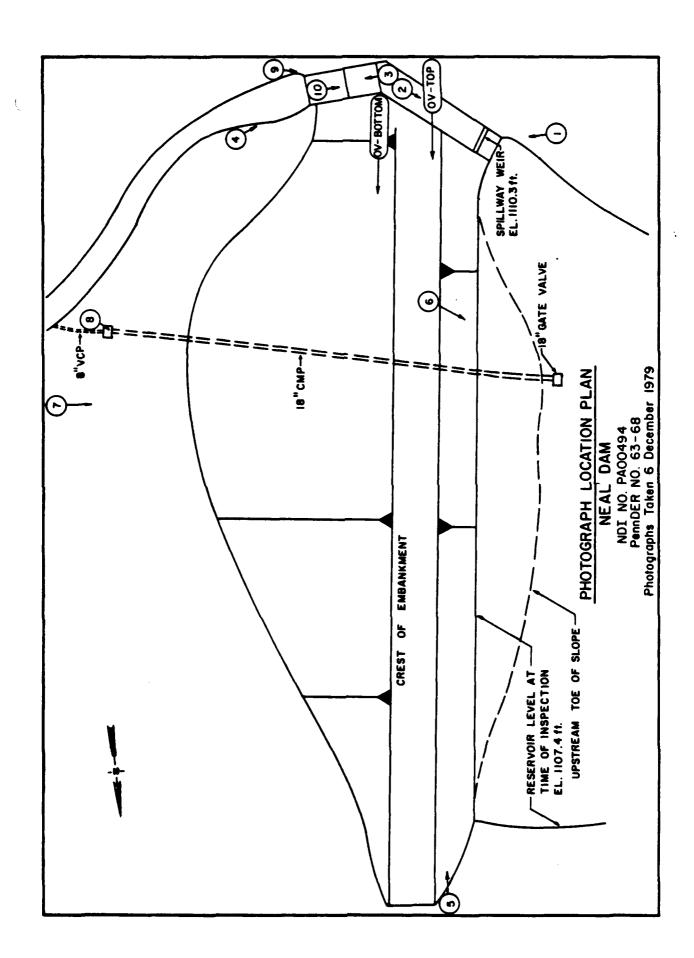
Overall View of Dam

Top Photo - Overall View of the Upstream Slope and (OV-T) Crest of the Dam from the Right Abutment Bottom Photo - Overall View of the Downstream Slope (OV-B) of the Dam from the Right Abutment

Photograph Location Plan

- Photo 1 View of the Approach to the Spillway
- Photo 2 View Looking Upstream at the Crest of the Spillway
- Photo 3 View Looking Downstream at Spillway Discharge Channel
- Photo 4 View Looking Upstream at Spillway Discharge Channel
- Photo 5 View of the Riprap and Crest of the Embankment from the Left Abutment
- Photo 6 View of the Valve Stem and Structure for the Outlet Conduit
- Photo 7 View Looking Upstream at the Downstream Slope
- Photo 8 Close-up View of the Discharge End of the Outlet Conduit
- Photo 9 Close-up View of the Erosion at the Right End of the Spillway Structure
- Photo 10 Close-up View of Several of the Cracks in the Spillway structure

Note: Photographs were taken on 6 December 1979.



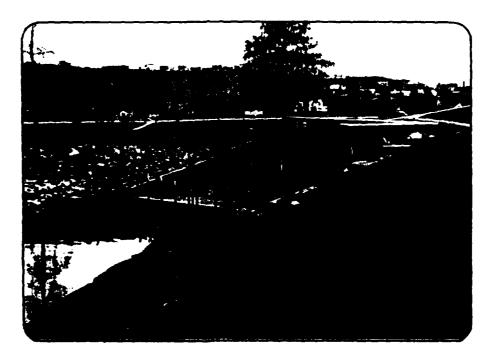


PHOTO 1. View of the Approach to the Spillway



PHOTO 2. View Looking Upstream at the Crest of the Spillway



PHOTO 3. View Looking Downstream at Spillway Discharge Channel



PHOTO 4. View Looking Upstream at Spillway Discharge Channel

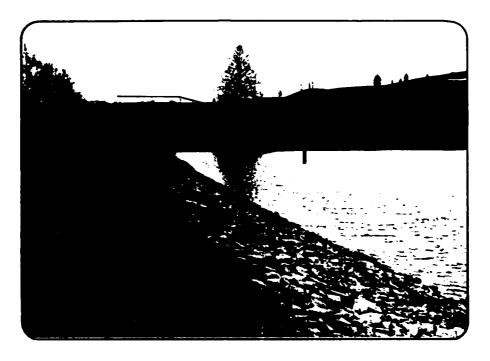


PHOTO 5. View of the Riprap and Crest of the Embankment from the Left Abutment



PHOTO 6. View of the Valve Stem and Structure for the Outlet Conduit



PHOTO 7. View Looking Upstream at the Downstream Slope

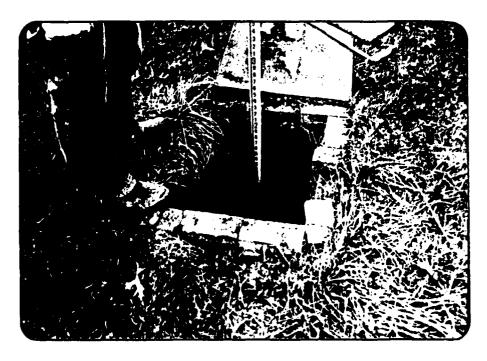


PHOTO 8. Close-up View of the Discharge End of the Outlet Conduit



PHOTO 9. Close-up View of the Erosion at the Right End of the Spillway Structure

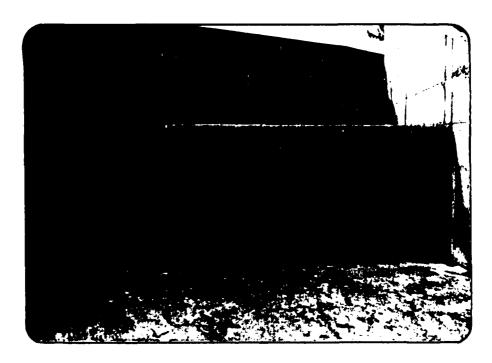


PHOTO 10. Close-up View of Several of the Cracks in the Spillway Structure

APPENDIX D

HYDROLOGIC AND HYDRAULIC COMPUTATIONS

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	DAM PROFILE AND	CROSS-SECTION	4		
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PREFACE

HYDROLOGIC AND HYDRAULIC COMPUTATIONS

The hydrologic determinations presented in this Phase I Inspection Report are based on the use of a Snyder's unit hydrograph developed by the U.S. Army Corps of Engineers. Due to the limited number of gaging stations available in this hydrologic region and the wide variations of watershed slopes, the Snyder's coefficients may yield results of limited accuracy for this watershed. As directed however, a further refinement of these coefficients is beyond the scope of this Phase I Investigation.

In addition, the conclusions presented pertain to present conditions, and the effect of future development on the hydrology has not been considered.

HYDROLOGY AND HYDRAULIC ANALYSIS DATA BASE

NAME OF DAM: NEAL DAM							
PROBABLE MAXIMUM PRECIPITATION	(PMP) = 24.2 IN	CHES/24 HOURS (1)	HOURS (1)				
STATION	1	2	3	4	5		
Station Description	NEAL DAM						
Orainage Area (square miles)	0.65						
Cumulative Drainage Area (square miles)	0.65						
Adjustment of PMF for Drainage Area (%)	Zone 7						
6 Hours 12 Hours 24 Hours 48 Hours 72 Hours	102 120 130 140						
Snyder Hydrograph Parameters							
Zone (3)	28						
c _p /c _t (4)	0.57/1.7						
L (miles) (5)	1.16						
L _{ca} (miles) (5)	0.57						
$t_p = C_t (L \cdot L_{ca})^{0.3}$ (hours)	1.5						
Spillway Data Crest Length (ft) Freeboard (ft) Discharge Coefficient Exponent	20 6 3.09 1.5						

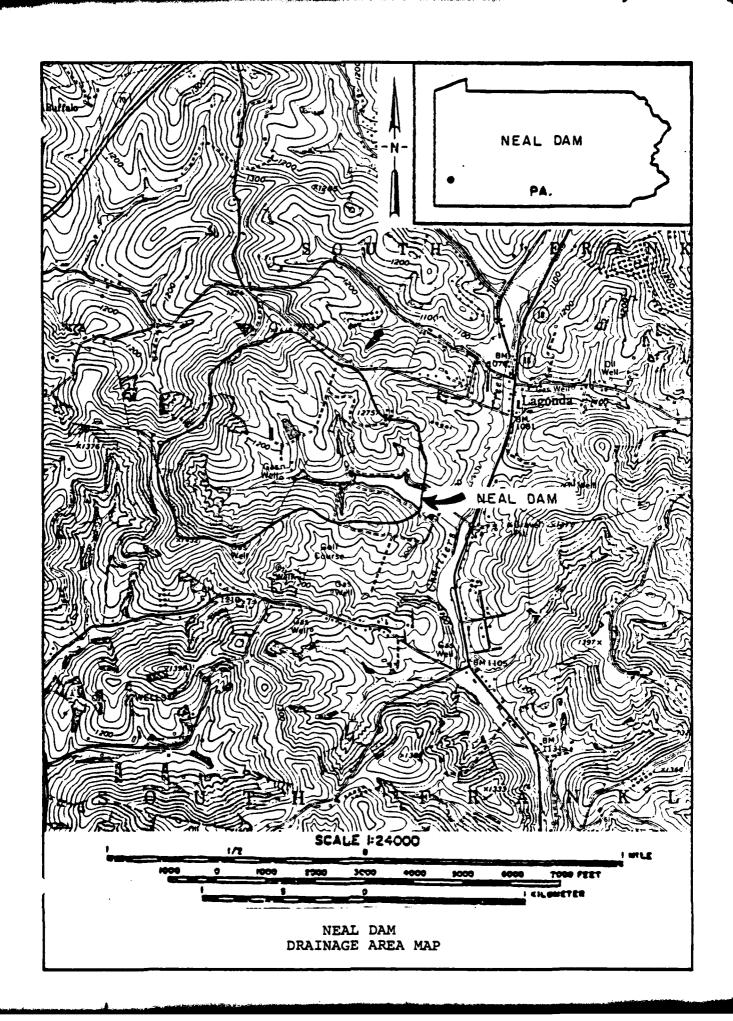
⁽¹⁾ Hydrometeorological Report 33 (Figure 1), U.S. Army, Corps of Engineers, 1956.

⁽²⁾ Hydrometeorological Report 33 (Figure 2), U.S. Army, Corps of Engineers, 1956.

⁽³⁾ Hydrological zone defined by Corps of Engineers, Baltimore District, for determining Snyder's Coefficients $(C_p$ and $C_t)$.

⁽⁴⁾ Snyder's Coefficients.

 $^{^{(5)}}L$ = Length of longest water course from outlet to basin divide. L_{ca} = Length of water course from outlet to point opposite the centroid of drainage area.



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POINT	STATION	ELEVATION
1	0-	1114.2
z	7.9	1113.0
3	14.5	1112.0
4	17.0	1111.58
5	17.0	1111.0
6	17.0	1110.44
7	17.0	1110.32
8	37.0	1110.32
9	37.0	1110.44
10	42.0	1111.0
"	47.6	1111.58
12	50. Z	1112.0
/3	58.3	1113.0
14	68.0	1114.2

MICHAEL BAKER, JR., INC.

THE BAKER ENGINEERS

Box 280 Beaver, Pa. 15009 Subject NEAL DAM

EMERGENCY SPILLWAY-RATING

_ S.O. No. <u>13547-00-ARA</u>-20

TABLE AT WEIR

Checked by WS Date 4 FEB 80

The rating table was dweloped assuming critical depth of the weir (control section). The equations used are from Chow's Open-Channel Hydraulics:

$$D = \frac{A}{T}$$
 (Equation 2-2, page 23)

V = \sqrt{QD (Equation 1-11, page 13)

Q= VA (Equation 1-1, page 5)

$$H_{V} = \frac{V^{2}}{2g} \left(page 3 \right)$$

E.G. = W.S. + H, (Figure 1-1, page 4)

where : D = hydraulic depth

A= cross section area

T= topwidth

g = acceleration due to gravity, 32.2 feet per second 2

Q= discharge

Hy = velocity head

E.G. = energy grade elevation

W.S. = water surface elevation

Upstream Water Surbox Elev. (feet,MSL)	Topwidth (feet)	Area (feet ²)	Depth (feet)	Velocity (fps)	Discharge (cls)	Velocity head (Feet)	E.G. Elev (feet, MSL)
	20 25 30.6 35.7 50.4 68.0 68.0 68.0	0° 2.4° 15.0° 31.1° 45.0° 88.1° 159.1° 213.5° 281.5° 349.5° 417.5°	1.2° 1.02° 1.26° 1.75° 2.34° 3.14° 4.14° 5.14 6.14°	0 1.97 4.40 5.72 6.37 7.50 8.68 10.0 11.6 12.9	0 4.7 66.0 171.9 286.6 660.8 1381 2135 3265 4509 5887	0 .06 .30 .30 .30 .30 .30 .30 .30 .30 .30 .30	0.32 0.50 12.09 12.63 13.87 13.87 16.55 18.09 19.58

Subject NEAL Dam. S.O. No. 13547-00-ARA-20 MICHAEL BAKER, JR., INC. EMERGENCY SPILLWAY - ROTING THE BAKER ENGINEERS Sheet No. 6 of 9 TABLE AT FIRST 1- FT. DROP Drawing No. ___ Box 280 _Checked by _*JAQ* Computed by ___ ALB _ Date 02/20/80 Beaver, Pa. 15009 1115 POINT STATION FLEVATION 10 1114.0 10___ 1/08.0 30 1105 ASSUME CRITICAL DEPTH: 30 HORIZONTAL DISTANCE (FEET) D= /T V= V& D Q VA H ZE EG WS+ H UPSTREAM WARE TOPWIDTH AREA Vecocity Discussor Vecocity Has DEPTH E.G. ELOV. SURFACE ELEV. Ifeet) (feet) (Feet) (Eps) __(22)__ [(ft. msl) _(feet, MSL)_ _ 20 0 01-01 -07 0~ 1108.0 1108.0 20 20 320.8 4 1.00 1109.0. ニュンゴ 5.47 1109.5 ___20 40 B.02 / 320.8 V 1110.0 __ 20 9.83 1771.0 1.50 20 11.35 / 908.0/ 2.00 80 7114.00 1112.0 12.89 - 1269.0 2500 __20 100 1113.0 __20 3.00 13.90 1668.00 1114:0 120 20 7713 4 1752 14 -3.10V 124 . 1114.2 75.01 / 27.01.4/ 3.500 _1115.0 -___20 140 __B 2568.0° 4.00° 3063.6° 4.50° 76.05 -1115.0 T 70 760 -1120.0V 17.02 3063.60 20 1117.0 180 1121.50

MICHAEL BAKER, JR., INC.

THE BAKER ENGINEERS

Box 280

Beaver, Pa. 15009

ENERGY GRADIENT ELEVATION VS. DISCHARGE

PATING SURVE AT FIRST GET

S.O. No. 13597-00-ARA-20

Sheet No. 7 of 9

Raffing Curve Drawing No. —

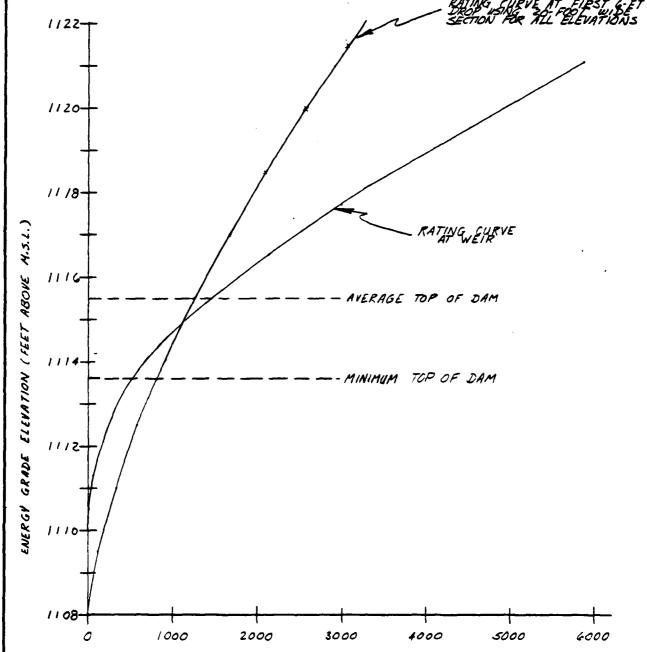
Dote Feb 4, 1980

ENERGY GRADIENT ELEVATION VS. DISCHARGE

1122—

PATING SURVE AT FIRST GET

SECTION FOR ALL ELEVATIONS



DISCHARGE (CFS)

Subject Neal Dam-Fmere 194 _ s.o. no. /3547-00-ARA-20 MICHAEL BAKER, JR., INC. THE BAKER ENGINEERS JAQ Date 12/6/79 Beaver, Pa. 15009 weir-2.4 A high, 1.0 A wide, downstream crest of slope cotoff wall - 2 A long' A wide to Constitute 6 ft vertical drop 6 At vertical drop -3 ft vertical dick into plumpe pool

White NEAL DAM MICHAEL BAKER, JR., INC. THE BAKER ENGINEERS PROFILE Box 280 Beaver, Pa. 15009 TOP OF DAM PROFILE (LOOKING DOWNSTREAM): PARKING LOT APPROXIMATE EDGE OF DAM 1120 -EL. 1/14.2 54 AUGRAGE TOP OF DAM ELEVATION = 1115.5 \$4 1115 CREST OF WEIR 1110 -(EL. 1110.32) 1105 -0 100 200 300 500 600 STATION (F4) CROSS SECTION: (AT STATION 2+00) NORMAL WATER LEVEL (EL. 1110.32) 1120-WATER LEVEL DURING INSPECTION / EL. 1115.7 34 1115-1110-1105-EL. 1099,3 St TOE OF EMBANKMENT ! (EL. 1991-154) 1100-JUNCTION BOX 1095-1090-18 INCH CMP 8 INCH VCP 1085-مای 100 200 250 150 STATION (74)

APPENDIX E

PLATES

CONTENTS

Plate 1 - Location Plan

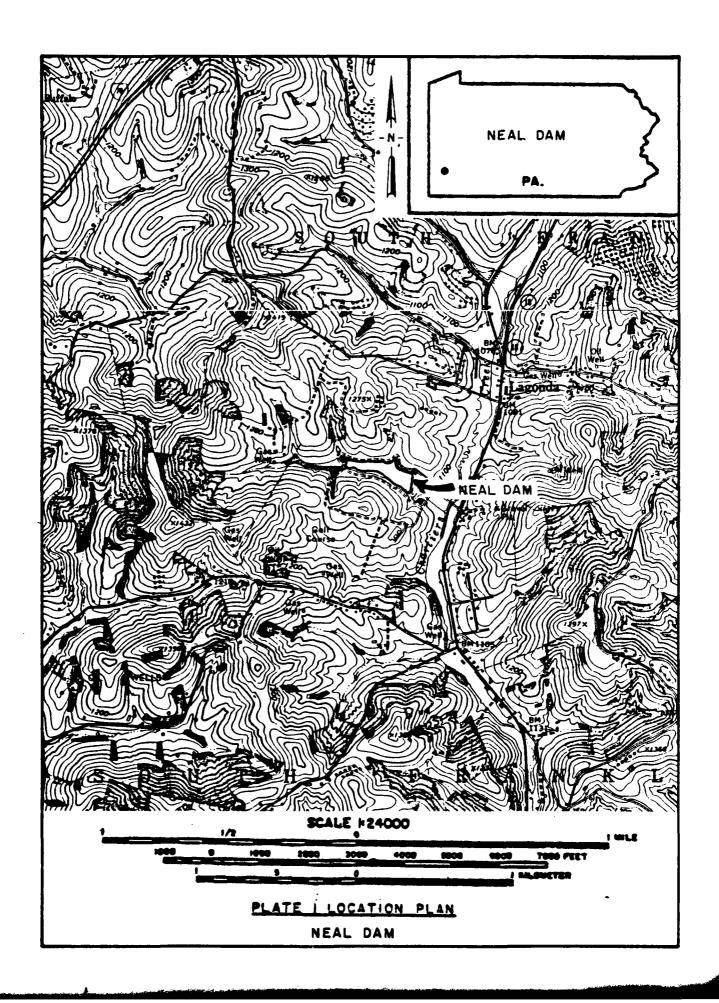
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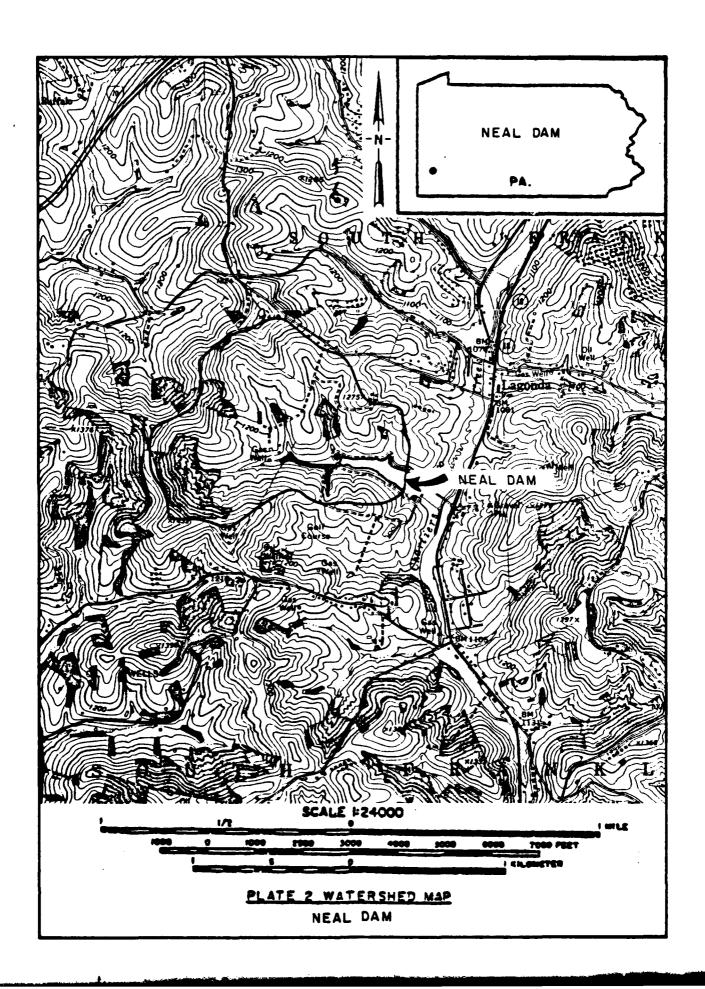
Plate 2 - Watershed Map

Plate 3 - General Plan and Cross-Section of Dam

Plate 4 - Profile of Dam and Spillway Details

Plate 5 - Topographic Survey of Dam and Reservoir Area

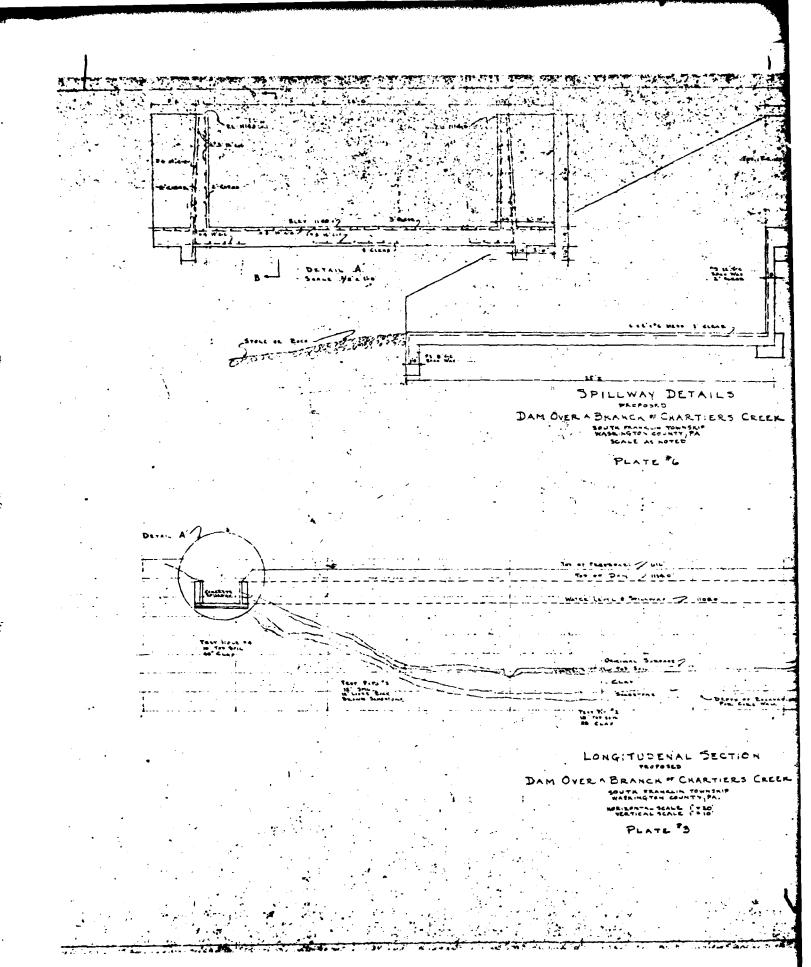


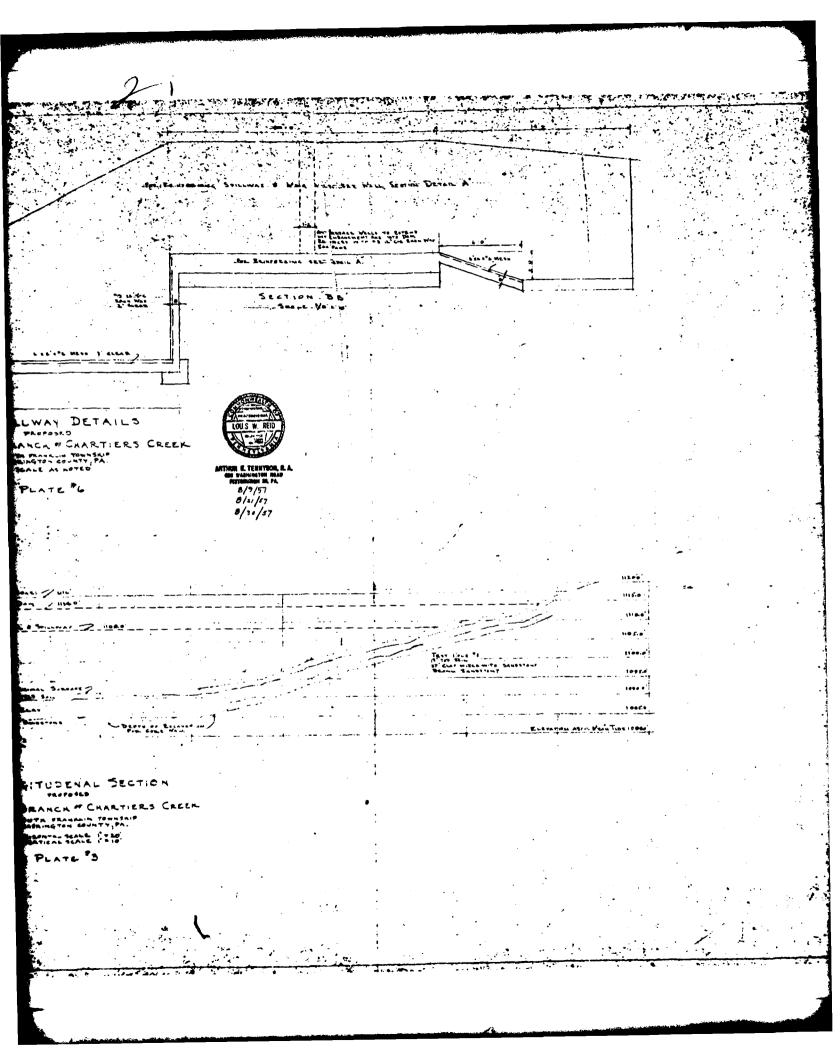


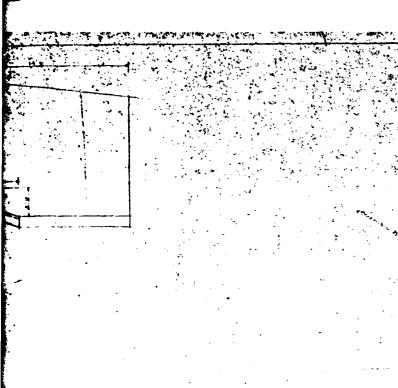
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CROSS URBLON BRIJCH OF CHARTIERS CREEK H FRANKLIN TOWNSHIP SHINGTON COUNTY, PA SEALE 1': 25' P-47 - 4 8/9/97 8/21/57 8/20/57

And Spanter DAM. OVER. A BRANCH . CHARTIERS CREEK SOUTH FRANKLIN TOWNSHIP WASKINGTON COUNTY, FA. CROSS SECTION 10 for Jour 50 C. A. C. Las Beneral Second S TROPOSED •





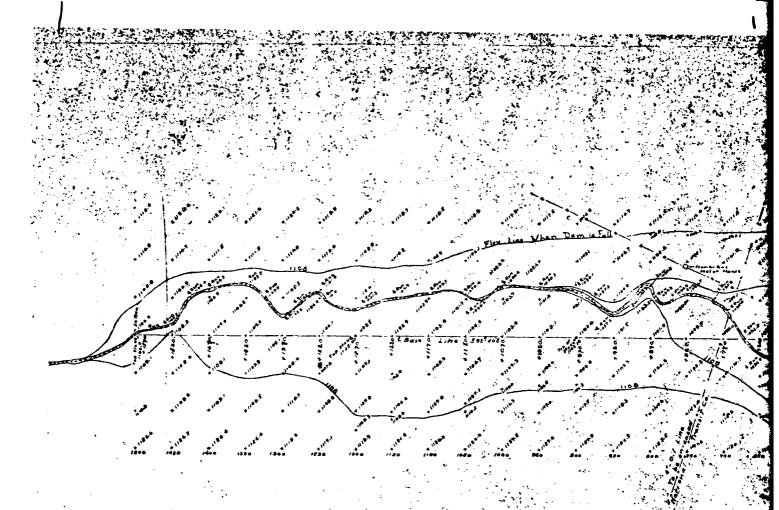


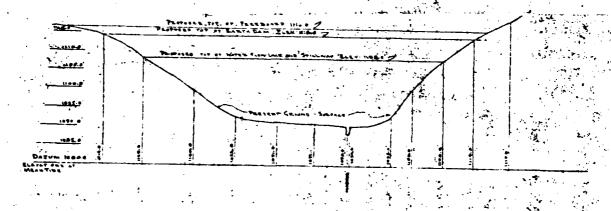
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PLATE 4



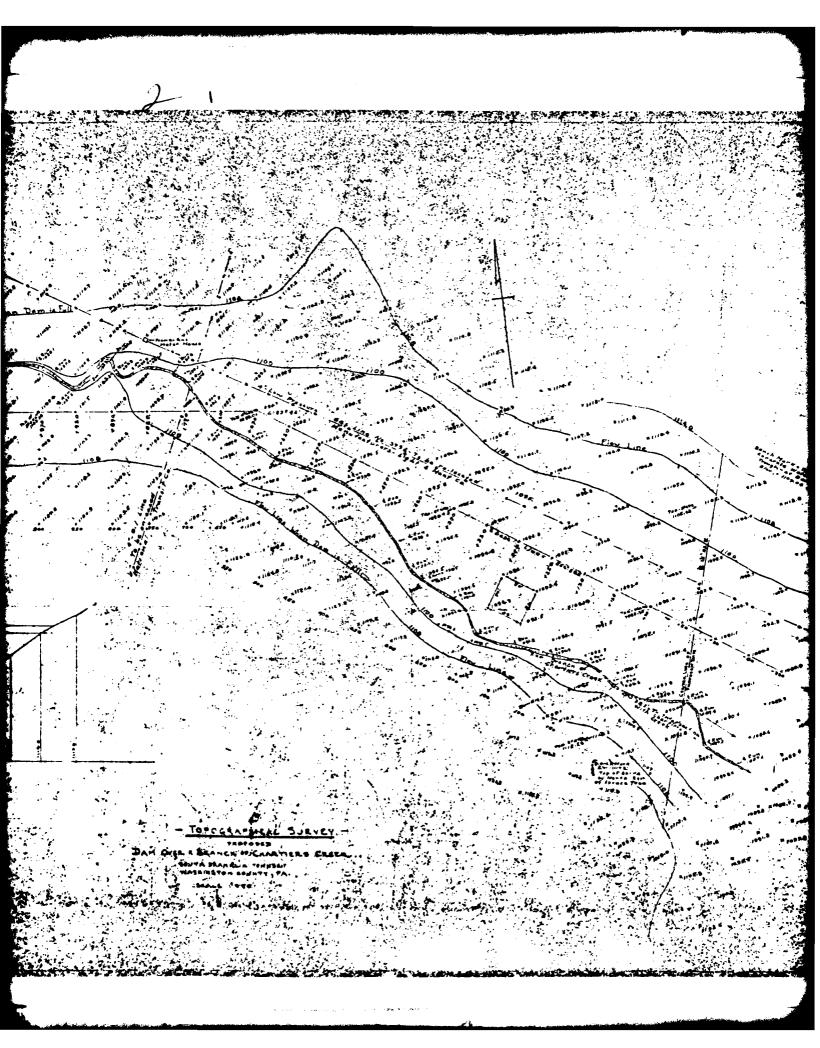


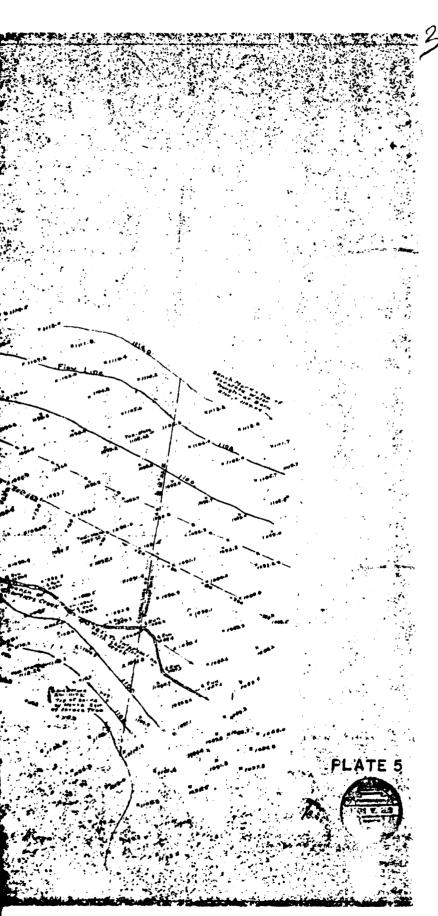


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APPENDIX F

REGIONAL GEOLOGY

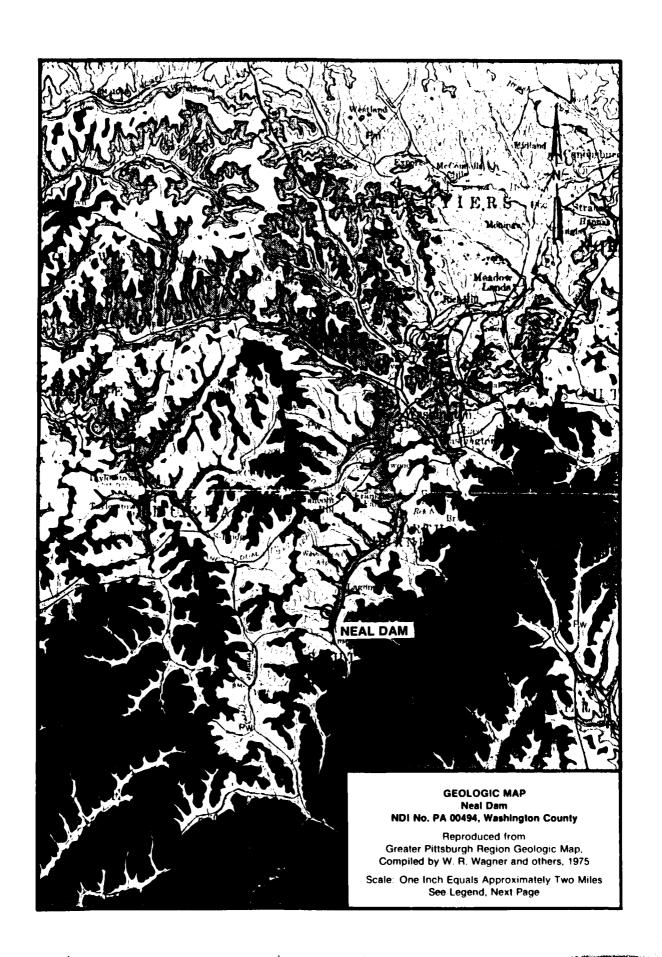
NEAL DAM NDI No. PA 00494, PennDER No. 63-68

REGIONAL GEOLOGY

The dam and reservoir are located in an unglaciated area of the Appalachian Plateaus Physiographic Province. The dam is located approximately 0.4 mile east of the axis of the Washington Anticline. According to the structure contour map for the Pittsburgh coal, the bedrock units are dipping approximately 60 to 80 feet to the southeast. (Reference: "Greater Pittsburgh Region Structure Contour Map of Allegheny, Armstrong, Beaver, Butler, Washington, and Westmoreland Counties, " compiled by W. R. Wagner and others, 1975.) Bedrock units below the dam are part of the Waynesburg Formation, Dunkard Group, Pennsylvanian System. This formation consists of cyclic sequences of sandstone, shale, limestone, and coal. The Waynesburg Formation contains the Waynesburg coalbed at the base of the formation. This coalbed is the marker which separates the bottom of the Dunkard Group from the top of the Monongahela Group. The overlying Washington Formation is shown outcropping above the elevation of the top of dam along the valley hillsides.

Located approximately 450 feet below the top of dam elevation is the Pittsburgh coal. The Pittsburgh coal mineral rights below the dam are identified as being owned by Republic Steel Corporation (Reference: "Greater Pittsburgh Region Mined Out Areas of the Pittsburgh Coal" by S. E. Curtis and others, 1975). The thickness of the Pittsburgh coal has been shown to be approximately 68 inches for the lower bench, a 9 inch parting, and 60 inches for the upper bench. Other coals above the Pittsburgh coal include in ascending order 1) Sewickley coal (absent), 2) Uniontown coal (represented by carbonaceous shaly mudstone), 3) Waynesburg coal (approximately 28 inches thick - note that at this location the Waynesburg coal is partially eroded by post-Early Permian erosion), 4) Waynesburg "A" coal (36 inch thick bed with 12 inches of coal), and 5) Washington coal on hillsides above dam (60 inch bed with 12 inches of coal). (Reference: "Coal-Bearing Upper Pennsylvanian and Lower Permian Rocks, Washington Area, Pennsylvania, by Henry L. Berryhill, Jr., Stanley P. Schweinfurth, and Bion H. Kent, United States Geological Survey Professional Paper No. 621, 1971.)

According to information on the original design drawings, four test pits excavated along the axis of the dam indicated that the foundation below the dam consisted of 12 to 18 inches of topsoil overlying 12 to 60 inches of clay. Bedrock below the soil in all cases was designated as brown sandstone.



GEOLOGY MAP LEGEND

GROUP FORMATION

DESCRIPTION

Alluvium		Ot	Sand, gravel, clay.
Т.	Terrace deposits		Sand, clay, gravel on terraces above present rivers; includes Carmichaels Formation.
	Greene		Cyclic sequences of sandstone, shale, red beds, thin limestones and coals.
DUNKARD	Washington	Pw	Cyclic sequences of sandstone, shale, limestone, and coal; contains Washington coal bed at base.
	Waynesburg	PPw	Cyclic sequences of sandstone, shale, limestone and coal; contains Waynesburg coal bed at base.
MONG	MONONGAHELA		Cyclic sequences of shale, limestone, sandstone and coal; contains Pittsburgh coal bed at base.
IGH	Casselman	Pcc	Cyclic sequence of sandstone, shale, red beds and thin limestone and coal.
P. AU	HON Ames Ames Glenshaw		
CONE			
			Cyclic sequences of sandstone, shale, red beds and thin limestone and coal; several fossil- iferous limestone; Ames limestone bed at top.
EZ	ENY		Cyclic sequences of shale, sandstone, limestone, and coal; contains Brookville coal at base and
LLEGHEN	Vanport		Upper Freeport coal at top; within group are the commercial Vanport limestone and Kittanning and Clarion coals.
	4		
POTT	POTTSVILLE		Sandstone and shale; contains some conglomerate and locally mineable coal.
	Mauch Chunk		Red and green shale with some sandstone; contains Wymps Gap and Lovalhanna lime – stones.
	Pocono		Sandstone and shale with Burgoon sandstone at top,

